

ME 315
Exam 2
8:00 -9:00 PM
Tuesday, March 10, 2009

- This is a closed-book, closed-notes examination. *There is a formula sheet at the back.*
- You must turn off all communications devices before starting this exam, and leave them off for the entire exam.
- Please write legibly and show all work for your own benefit. Please show your final answers in the boxes provided.
- State all assumptions.
- Please arrange all your sheets in the correct order. Make sure they are all included.

Name: _____
Last **First**

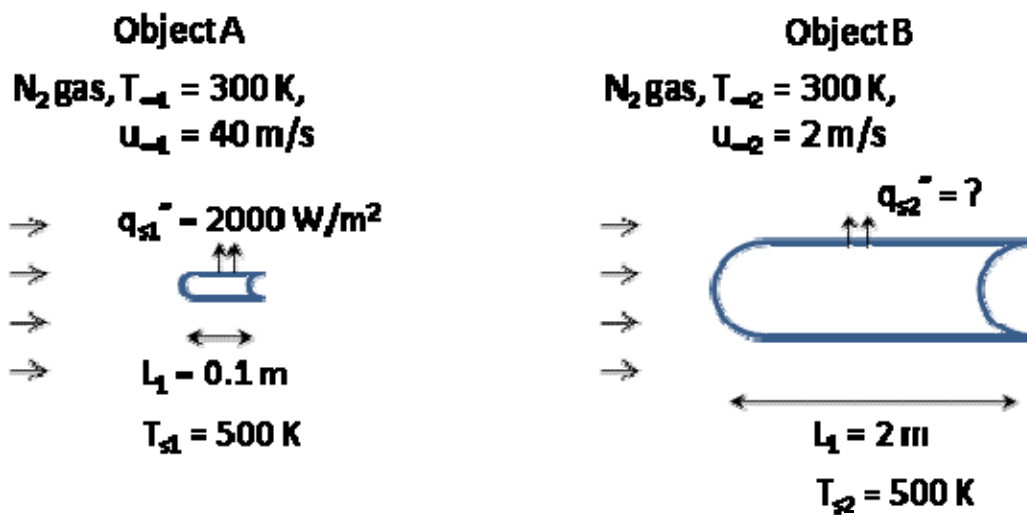
CIRCLE YOUR DIVISION

Div. 1 (9:30 am)
Prof. Murthy

Div. 2 (12:30 pm)
Prof. Choi

Problem	Score
1 (20 Points)	
2 (40 Points)	
3 (40 Points)	
Total (100 Points)	

1. Consider the following two objects with the same geometry but different sizes exposed to nitrogen gas. The two objects are at 500 K, while the N₂ gas has a temperature of 300 K.



All properties may be evaluated at 400 K: For nitrogen, you are given thermal conductivity, $k = 26.0 \times 10^{-3} \text{ W/mK}$; density, $\rho = 1.0 \text{ kg/m}^3$; specific heat, $c_p = 1000 \text{ J/kgK}$; kinematic viscosity, $\nu = 18.2 \times 10^{-6} \text{ m}^2/\text{s}$.

With given conditions, the heat flux in object A is found to be $q_{s1}'' = 2,000 \text{ W/m}^2$. What is the average convective heat transfer coefficient (h_2) and heat flux in q_{s2}'' in object B?

$h_2 =$	$\text{W/m}^2\text{K}$
$q_{s2}'' =$	W/m^2

Solution

$$\overline{Nu} = f(Re, Pr) = \frac{h L_c}{k}; \quad Re = \frac{\rho U L_c}{\mu} \quad Pr = \frac{\nu}{\alpha}$$

$$\alpha_1 = \alpha_2 \rightarrow Pr_1 = Pr_2$$

$$20 \cdot L_{c1} = L_{c2}, U_1 = 20 \cdot U_2 \rightarrow Re_1 = Re_2$$

$$\therefore \overline{Nu}_1 = \overline{Nu}_2 \rightarrow \frac{h_1 L_{c1}}{k} = \frac{h_2 L_{c2}}{k}$$

$$\therefore h_2 = \frac{h_1 L_{c1}}{L_{c2}} = \frac{h_1 L_{c1}}{20 \cdot L_{c1}} = \frac{h_1}{20}$$

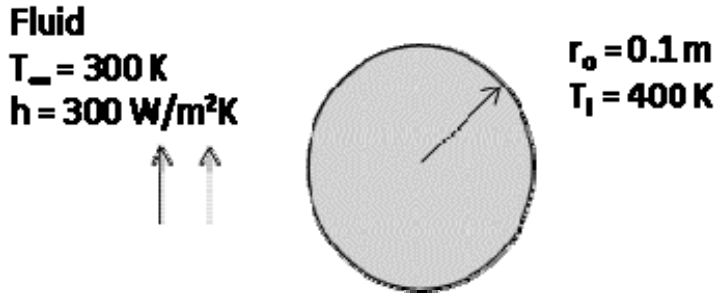
$$q_1'' = h_1 \cdot (T_{s,1} - T_\infty) = h_1 \cdot (500 - 300) = 2000 \text{ W/m}^2 \rightarrow h_1 = 10 \text{ W/m}^2 - K$$

$$\therefore h_2 = \frac{h_1}{20} = 0.5 \text{ W/m}^2 - K$$

$$q_2'' = h_2 \cdot (T_{s,2} - T_\infty) = (0.5 \text{ W/m}^2 - K) \cdot (500 - 300) K = 100 \text{ W/m}^2$$

$$\therefore q_2'' = 100 \text{ W/m}^2$$

2. A spherical metal ball of a radius, $r_o = 0.1$ m is initially at $T_i = 400$ K. At $t = 0$, the ball is submerged in a fluid, where convective heat transfer coefficient, h , is $300 \text{ W/m}^2\text{K}$ and the temperature, T_∞ , is 300 K. This ball is assumed to have a uniform temperature at any time.



You are given the following properties of the ball: Thermal conductivity, $k = 30 \text{ W/mK}$; density, $\rho = 9000 \text{ kg/m}^3$; heat capacity, $c_p = 500 \text{ J/kgK}$.

(i) Determine thermal time constant (τ_t) of the ball and the temperature of the ball at $t = \tau_t$.

$\tau_t =$	second
T =	K

(ii) Evaluate the validity of the uniform temperature assumption. Provide reasoning.

Valid ? Invalid ? (Circle one.)
Reason:

If your answer states Valid, stop here and proceed to problem #3. If it is Invalid, go to (iii) on the next page.

(iii) Determine the temperature at the center of the ball at $t = \tau_t$.

$T = \quad \quad K$

Solution

(i)

$$\tau_t = \frac{\rho V C_p}{h_{conv} A_s}$$

$$V = \frac{4}{3} \pi r_o^3$$

$$A_s = 4 \pi r_o^2$$

$$\therefore \tau_t = \frac{\rho V C_p}{h_{conv} A_s} = \frac{\rho \frac{4}{3} \pi r_o^3 C_p}{h_{conv} 4 \pi r_o^2} = \frac{\rho r_o C_p}{3 h_{conv}} = \frac{(9000 \text{ kg/m}^3) \cdot (0.1 \text{ m}) \cdot (500 \text{ J/kg-K})}{3 \cdot (300 \text{ W/m}^2 \cdot \text{K})} = 500 \text{ sec}$$

$\therefore \tau_t = 500 \text{ sec}$

$$\frac{\theta}{\theta_i} = \frac{T - T_\infty}{T_i - T_\infty} = \exp\left(-\frac{t}{\tau_t}\right); \quad t = \tau_t \quad \therefore \frac{t}{\tau_t} = 1$$

$$\frac{T - T_\infty}{T_i - T_\infty} = \exp(-1)$$

$$\therefore T = T_\infty + (T_i - T_\infty) \cdot \exp(-1) = 300 + (400 - 300) \cdot \exp(-1) = 336.788 \text{ K}$$

$\therefore T_{t=\tau_t} = 336.788 \text{ K}$

(ii)

$$Bi = \frac{h_{conv} \cdot L_c}{k_{solid}} \quad ; \quad L_c = \frac{r_o}{3} = \frac{0.1 \text{ m}}{3}$$

$$\therefore Bi = \frac{(300 \text{ W/m}^2 - K) \cdot \left(\frac{0.1 \text{ m}}{3}\right)}{(30 \text{ W/m} - K)} = 0.333 > 0.1$$

$\therefore Invalid \text{ because } Bi = 0.333 > 0.1$

(iii)

$$Bi = \frac{h_{conv} \cdot r_o}{k_{solid}} = \frac{(300 \text{ W/m}^2 - K) \cdot (0.1 \text{ m})}{30 \text{ W/m} - K} = 1.0$$

From the Table 5.1,

$$\zeta_1 = 1.5708, \quad C_1 = 1.2732$$

$$\theta_o^* = \frac{T - T_\infty}{T_i - T_\infty} = C_1 \cdot \exp(-\zeta_1 \cdot Fo)$$

$$Fo = \frac{\alpha t}{r_o^2} \quad ; \quad \alpha = \frac{k}{\rho \cdot C_p}$$

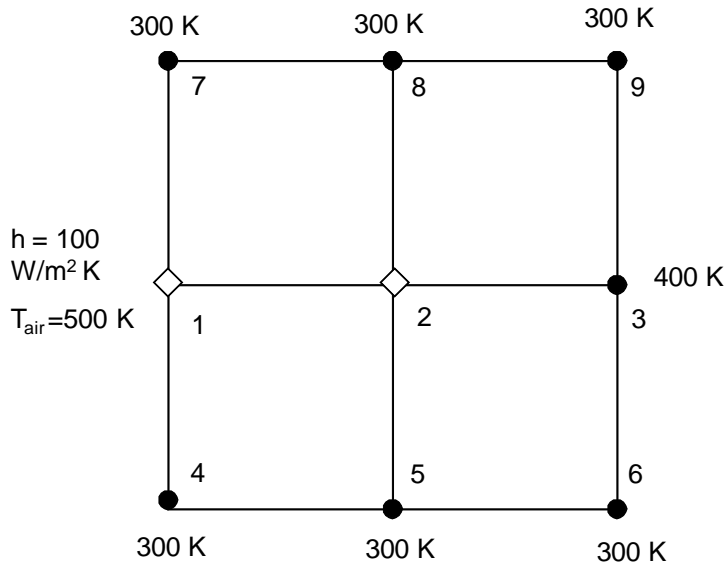
$$\therefore Fo = \frac{k}{\rho \cdot C_p} \cdot \frac{t}{r_o^2} = \frac{(30 \text{ W/m} - K)}{(9000 \text{ kg/m}^3) \cdot (500 \text{ J/kg} - K)} \cdot \frac{(500 \text{ sec})}{(0.1 \text{ m})^2} = 0.333$$

$$\therefore \theta_o^* = \frac{T - T_\infty}{T_i - T_\infty} = \frac{T - 300}{400 - 300} = (1.2732) \cdot \exp[-(1.5708)^2 \cdot (0.333)] = 0.5598$$

$\therefore T_{r=0,500\text{sec}} = 355.983 \text{ K}$

3. Consider unsteady heat conduction in a 2D square domain of side 2 m, as shown below. The domain is meshed with a square mesh with $\Delta x = \Delta y = 1$ m. The initial temperature at all grid points is 300 K. At time $t=0$, the boundary conditions shown below are applied. You are asked to determine how the temperatures of grid points 1 and 2 change with time using an explicit time stepping scheme.

You are given the following material properties:
 $\rho = 2000 \text{ kg/m}^3$ $k = 100 \text{ W/mK}$ $C_p = 300 \text{ J/kgK}$



- (i) You are given the choice of two time steps, $\Delta t = 500$ s and $\Delta t = 2000$ s. Which one would you choose, and why?

$\Delta t =$ seconds
Reason:

- (ii) Develop analytical equations for T_1 and T_2 at time step $t = \Delta t$ in terms of neighbor temperatures, material properties and mesh parameters. Show analytical expressions for the discrete equations here.

$T_1 =$
$T_2 =$

(iii) Using the value of Δt you chose in part (i), determine the numerical values of the coefficients in the discrete equations derived in part (ii).

$T_1 =$ $T_2 =$
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(iv) Find the numerical values of the temperatures T_1 and T_2 at $t = \Delta t$ using the explicit scheme.

$T_1 (t = \Delta t) =$ $T_2 (t = \Delta t) =$
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Solution

(i)

For 2-D, the stability limit is $Fo \leq \frac{1}{4}$

$$Fo = \frac{\alpha \cdot \Delta t}{(\Delta x)^2}; \alpha = \frac{k}{\rho \cdot c_p} = \frac{100 \text{ W/m-K}}{(2000 \text{ kg/m}^3) \cdot (300 \text{ J/kg-K})} = 0.000167 \text{ m}^2/\text{s}$$

$$\therefore Fo = \frac{(0.000167 \text{ m}^2/\text{s}) \cdot \Delta t}{(1 \text{ m})^2} \leq \frac{1}{4} \rightarrow \Delta t \leq 1500 \text{ s}$$

$\therefore \Delta t = 500 \text{ sec is suitable}$

(ii)

Node 1

$$\dot{E}'_{in} - \dot{E}'_{out} - \dot{E}'_{gen} = \dot{E}'_{st} \quad ; \quad \dot{E}'_{in} = q'_E + q'_W + q'_S + q'_N \quad \dot{E}'_{out} = 0 \quad \dot{E}'_{gen} = 0$$

$$q'_E = -k \frac{\Delta y}{\Delta x} (T_1^p - T_2^p) \quad q'_W = h \Delta y (T_{air} - T_1^p)$$

$$q'_S = -k \frac{\Delta x}{2 \cdot \Delta y} (T_1^p - T_4^p) \quad q'_N = -k \frac{\Delta x}{2 \cdot \Delta y} (T_1^p - T_7^p)$$

$$\dot{E}'_{st} = \rho \cdot c_p \cdot \frac{\Delta x}{2} \cdot \Delta y \cdot \frac{T_1^{p+1} - T_1^p}{\Delta t}$$

$$\therefore q'_E + q'_W + q'_S + q'_N = \dot{E}'_{st}$$

$$k \frac{\Delta y}{\Delta x} (T_2^p - T_1^p) + h \Delta y (T_{air} - T_1^p) + k \frac{\Delta x}{2 \cdot \Delta y} (T_4^p - T_1^p) + k \frac{\Delta x}{2 \cdot \Delta y} (T_7^p - T_1^p) = \rho \cdot c_p \cdot \frac{\Delta x}{2} \cdot \Delta y \cdot \frac{T_1^{p+1} - T_1^p}{\Delta t}$$

$$k (T_2^p - T_1^p) + h \Delta y (T_{air} - T_1^p) + \frac{k}{2} (T_4^p - T_1^p) + \frac{k}{2} (T_7^p - T_1^p) = \rho \cdot c_p \cdot \frac{\Delta x}{2} \cdot \Delta y \cdot \frac{T_1^{p+1} - T_1^p}{\Delta t}$$

$$T_1^{p+1} = T_1^p + \frac{2 \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x \cdot \Delta y} \cdot [k (T_2^p - T_1^p) + h \Delta y (T_{air} - T_1^p) + \frac{k}{2} (T_4^p - T_1^p) + \frac{k}{2} (T_7^p - T_1^p)]$$

$$= T_1^p + 2 \cdot Fo (T_2^p - T_1^p) + \frac{2 \cdot h \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x} (T_{air} - T_1^p) + Fo \cdot (T_4^p - T_1^p) + Fo \cdot (T_7^p - T_1^p)$$

$$(\because Fo = \frac{\alpha \cdot \Delta t}{\Delta x \cdot \Delta y} = \frac{\alpha \cdot \Delta t}{(\Delta x)^2} \quad \text{and} \quad \alpha = \frac{k}{\rho \cdot c_p})$$

$$\therefore T_1^{p+1} = T_1^p + \frac{2 \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x \cdot \Delta y} \cdot [k (T_2^p - T_1^p) + h \Delta y (T_{air} - T_1^p) + \frac{k}{2} (T_4^p - T_1^p) + \frac{k}{2} (T_7^p - T_1^p)]$$

or

$$T_1^{p+1} = T_1^p + 2 \cdot Fo (T_2^p - T_1^p) + \frac{2 \cdot h \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x} (T_{air} - T_1^p) + Fo \cdot (T_4^p - T_1^p) + Fo \cdot (T_7^p - T_1^p)$$

Node 2

$$T_2^{p+1} = (1 - 4 \cdot Fo) \cdot T_2^p + Fo \cdot (T_1^p + T_3^p + T_5^p + T_8^p)$$

$$\therefore T_2^{p+1} = (1 - 4 \cdot Fo) T_2^p + Fo (T_1^p + T_3^p + T_5^p + T_8^p)$$

(iii)

For $\Delta t = 500 \text{ sec}$, $Fo = 0.083$

$$\frac{\alpha \cdot \Delta t}{\Delta x \cdot \Delta y} = \frac{\alpha \cdot \Delta t}{(\Delta x)^2} = Fo = 0.083 \quad ; \quad \Delta x = \Delta y$$

$$\frac{2 \cdot h \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x} = \frac{2 \cdot (100 \text{ W/m}^2 - \text{K}) \cdot (500 \text{ sec})}{(2000 \text{ kg/m}^3) \cdot (300 \text{ J/kg-K}) \cdot (1 \text{ m})} = 0.1667$$

$$1 - 4 \cdot Fo = 1 - 4 \cdot 0.083 = 0.6667$$

$$\begin{aligned} T_1^{p+1} &= T_1^p + 2 \cdot Fo (T_2^p - T_1^p) + \frac{2 \cdot h \cdot \Delta t}{\rho \cdot c_p \cdot \Delta x} (T_{air} - T_1^p) + Fo \cdot (T_4^p - T_1^p) + Fo \cdot (T_7^p - T_1^p) \\ &= T_1^p + 2 \cdot (0.083) \cdot (T_2^p - T_1^p) + (0.1667) \cdot (T_{air} - T_1^p) + (0.083) \cdot (T_4^p - T_1^p) + (0.083) \cdot (T_7^p - T_1^p) \end{aligned}$$

$$\begin{aligned} T_2^{p+1} &= (1 - 4 \cdot Fo) \cdot T_2^p + Fo \cdot (T_1^p + T_3^p + T_5^p + T_8^p) \\ &= [1 - 4 \cdot (0.083)] \cdot T_2^p + (0.083) \cdot (T_1^p + T_3^p + T_5^p + T_8^p) \\ &= (0.6667) \cdot T_2^p + (0.083) \cdot (T_1^p + T_3^p + T_5^p + T_8^p) \end{aligned}$$

$$\therefore T_1^{p+1} = T_1^p + 2 \cdot (0.083) \cdot (T_2^p - T_1^p) + (0.1667) \cdot (T_{air} - T_1^p) + (0.083) \cdot (T_4^p - T_1^p) + (0.083) \cdot (T_7^p - T_1^p)$$

$$T_2^{p+1} = (0.6667) \cdot T_2^p + (0.083) \cdot (T_1^p + T_3^p + T_5^p + T_8^p)$$

(iv)

$$\begin{aligned} T_1^{p+1} &= T_1^p + 2 \cdot (0.083) \cdot (T_2^p - T_1^p) + (0.1667) \cdot (T_{air} - T_1^p) + (0.083) \cdot (T_4^p - T_1^p) + (0.083) \cdot (T_7^p - T_1^p) \\ &= 300 + 2 \cdot (0.083) \cdot (300 - 300) + (0.1667) \cdot (500 - 300) + (0.083) \cdot (300 - 300) + (0.083) \cdot (300 - 300) \\ &= 333.34 \text{ K} \end{aligned}$$

$$\begin{aligned} T_2^{p+1} &= (0.6667) \cdot T_2^p + (0.083) \cdot (T_1^p + T_3^p + T_5^p + T_8^p) \\ &= (0.6667) \cdot (300) + (0.083) \cdot (300 + 400 + 300 + 300) \\ &= 307.91 \text{ K} \end{aligned}$$

$\therefore T_1^{p+1} = 333.34 \text{ K}$	$T_2^{p+1} = 307.91 \text{ K}$
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