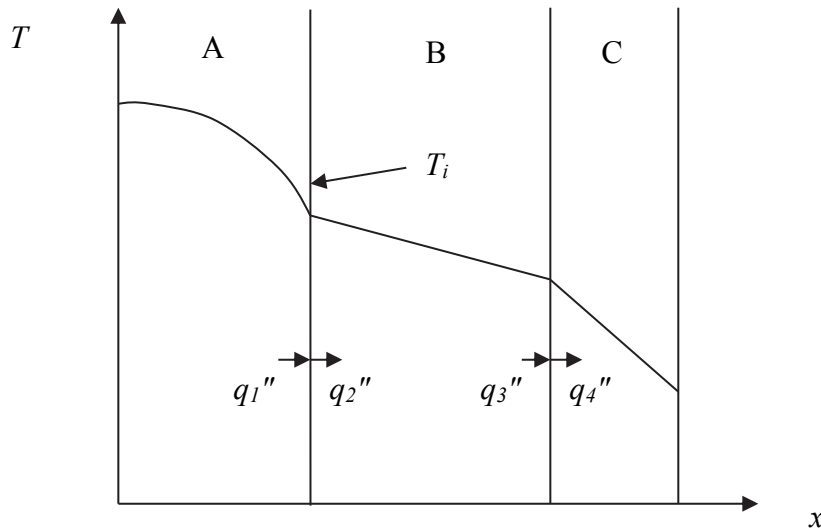


## Problem 1 [35 points]

The steady-state temperature distribution in a 1-D composite plane wall of three different materials, each of constant but different thermal conductivity,  $k_A$ ,  $k_B$ , and  $k_C$ , is shown in the figure below. Material A has a uniform volumetric heat generation  $\dot{q}$  [ $\text{W}/\text{m}^3$ ]. The thicknesses of the walls in A, B, and C are  $L_A$ ,  $L_B$ , and  $L_C$ , respectively. The left side of the wall is insulated, and the right side of the wall is subjected to convection cooling, with  $T_\infty$  and  $h$ .

- Comment on the relative magnitudes of  $q_1''$  and  $q_2''$ , and relative magnitudes of  $q_3''$  and  $q_4''$ . Provide a brief justification.
- Comment of the relative magnitudes of  $k_A$  and  $k_B$ , and of  $k_B$  and  $k_C$ , and provide a brief justification.
- Sketch heat flux  $q''$  as a function of  $x$ , in the figure on the next page.
- Find the expression of the temperature at the interface between wall A and wall B,  $T_i$ , in terms of given parameters  $\dot{q}$ ,  $L_A$ ,  $L_B$ ,  $L_C$ ,  $k_A$ ,  $k_B$ ,  $k_C$ ,  $h$ , and  $T_\infty$ .



List your assumptions below. [3 pts]

- Radiation Negligible
- Constant resistances or material properties
- No contact thermal resistance

Start you answer to part (a) here. [6 pts]

$$q_1'' = q_2''$$

$$q_3'' = q_4''$$

Due to energy balance or energy conservation at the interfaces

**Problem 1 – continued**

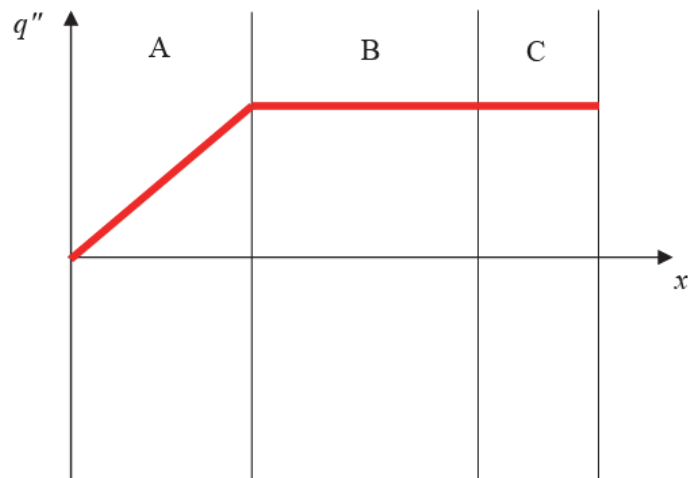
**Start your answer to part (b) here. [6 pts]**

$$\text{From (a), } q_1'' = q_2'' \Rightarrow -k_A \left. \frac{dT}{dx} \right|_A = -k_B \left. \frac{dT}{dx} \right|_B$$

$$\text{Also, from the figure } \left. \frac{dT}{dx} \right|_A > \left. \frac{dT}{dx} \right|_B$$

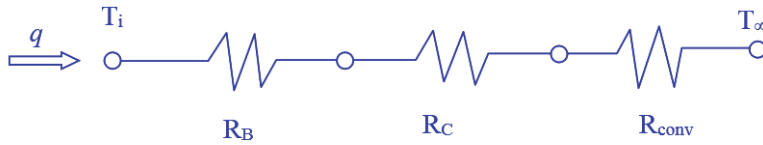
$$\text{We can get } \begin{aligned} k_A &< k_B \\ k_B &> k_C \end{aligned}$$

**(c) Plot  $q''$  vs.  $x$  in the figure below. [10 pts]**



**Problem 1 – continued**

**Start your answer to part (d) here. [10 pts]**



Apply energy balance:  $\dot{q} \cdot A \cdot L_A = q$

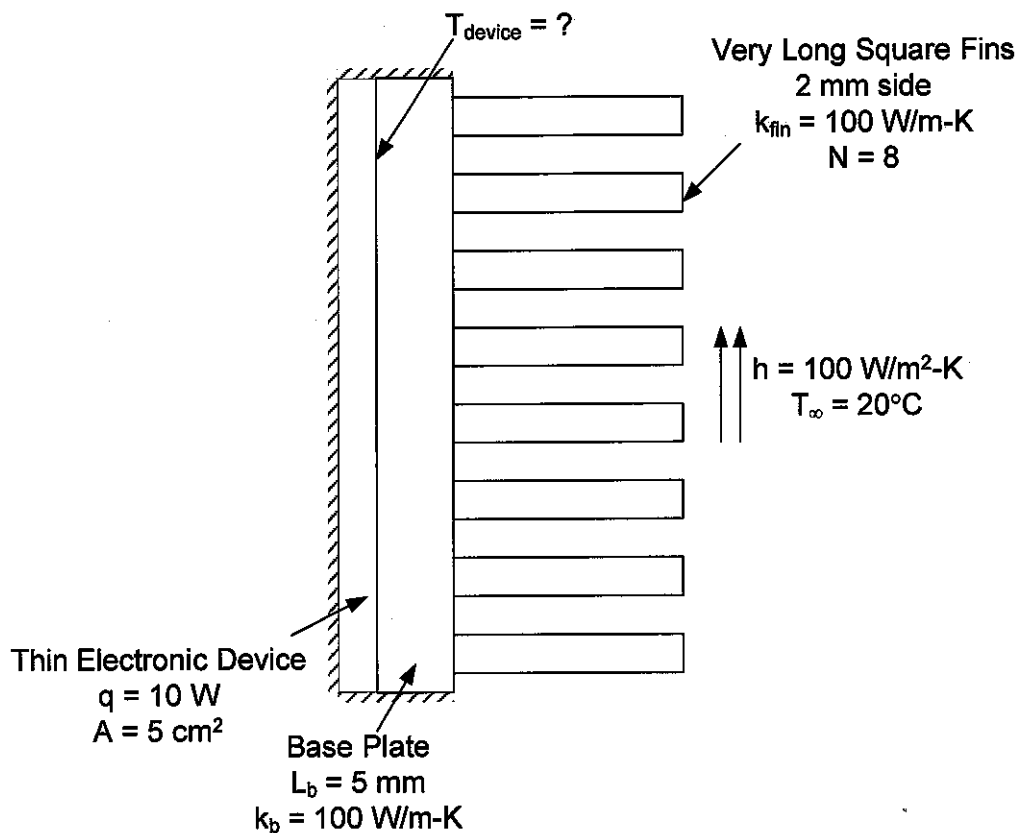
$$\Rightarrow q = \frac{T_i - T_\infty}{\frac{L_B}{k_B A} + \frac{L_C}{k_C A} + \frac{1}{hA}}$$

$$\Rightarrow T_i = \dot{q} L_A \left( \frac{L_B}{k_B} + \frac{L_C}{k_C} + \frac{1}{h} \right) + T_\infty$$

**Problem 2 [35 points]**

A thin electronic device of cross-sectional area  $5 \text{ cm}^2$  dissipates  $10 \text{ W}$  of heat. The device is insulated on one side. A heat sink of the same surface area is directly attached to the electronic device. Thermal conductivity of the heat sink material is  $100 \text{ W/(m}\cdot\text{K)}$ . The base plate of the heat sink has a thickness of  $5 \text{ mm}$ . Eight infinitely long fins are attached to the base plate and the fins have a square cross-section of  $2 \text{ mm}$  side. Air with ambient temperature of  $20^\circ\text{C}$  and convective heat transfer coefficient  $100 \text{ W/(m}^2\text{K)}$  flows on the heat sink.

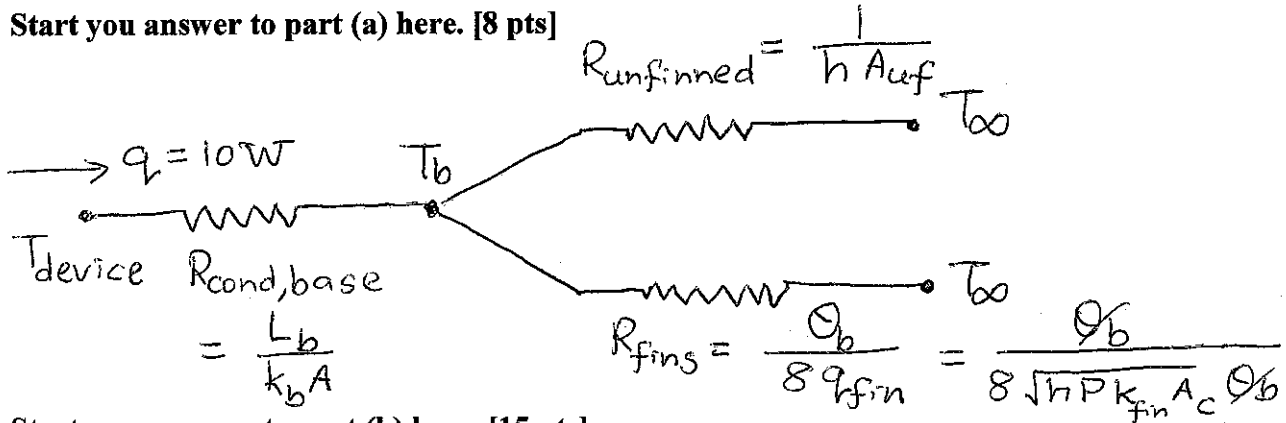
- Draw a thermal circuit for the system and label all resistances.
- Determine temperature ( $^\circ\text{C}$ ) at the interface between the device and the base plate.
- Calculate the effectiveness of a single fin.
- What is the value of efficiency of a single fin?



- List your assumptions below. [2 pts] \* Steady state
- \* No contact resistance between device and base plate
  - \* No contact resistance between base plate and fins
  - \* 1-D conduction through base plate and fins
  - \*  $h_{\text{unfinned}} = h_{\text{fin}} = h$
  - \* Uniform convection on exposed surfaces
  - \* Ignore radiation from exposed surfaces

**Problem 2 – continued**

Start your answer to part (a) here. [8 pts]



Start your answer to part (b) here. [15 pts]

Considering thermal circuit:

$$q = \frac{T_{\text{device}} - T_{\infty}}{R_{\text{eq}}}$$

$$R_{\text{cond, base}} = \frac{L_b}{k_b A} = \frac{5 \times 10^{-3} \text{ m}}{\frac{100 \text{ W}}{\text{m-K}} \times 5 \times 10^{-4} \text{ m}^2} = 0.1 \frac{\text{K}}{\text{W}}$$

$$R_{\text{unfinned}} = \frac{1}{h A_{\text{surf}}} = \frac{1}{h (A - 8 w^2)} = \frac{1}{100 \frac{\text{W}}{\text{m}^2 \text{K}} \times (5 - 8 \times (0.2)^2) \times 10^{-4} \text{ m}^2} = 21.4 \frac{\text{K}}{\text{W}}$$

$$R_{\text{fins}} = \frac{1}{8 \sqrt{\frac{h P k_{\text{fin}} A_c}{4 w}}} = \frac{1}{8 \sqrt{100 \frac{\text{W}}{\text{m}^2 \text{K}} \times 8 \times 10^{-3} \text{ m} \times 100 \frac{\text{W}}{\text{m-K}} \times (0.2)^2 \times 10^{-4} \text{ m}^2}} = 7 \frac{\text{K}}{\text{W}}$$

$$R_{\text{eq}} = R_{\text{cond, base}} + (R_{\text{unfinned}} \parallel R_{\text{fins}}) = 5.38 \frac{\text{K}}{\text{W}}$$

Temperature at the interface between the device and the base plate:  $T_{\text{device}} = T_{\infty} + q R_{\text{eq}}$

$$T_{\text{device}} = 20^{\circ}\text{C} + 10 \text{ W} \times 5.38 \frac{\text{K}}{\text{W}}$$

$$\boxed{T_{\text{device}} = 73.8^{\circ}\text{C}}$$

Circle your division: 1 2 3 4 Name \_\_\_\_\_

**Problem 2 – continued**

**Start your answer to part (c) here. [6 pts]**

$$\text{Effectiveness} \equiv \epsilon_{fin} = \frac{q_{fin}}{q_{w/o\ fin}} = \frac{\sqrt{hPk_{fin}A_c} \theta_b}{hA_c \theta_b} = \sqrt{\frac{Pk_{fin}}{hA_c}}$$

$$\epsilon_{fin} = \sqrt{\frac{8 \times 10^{-3} \text{ m} \times 100 \frac{\text{W}}{\text{m} \cdot \text{K}}}{100 \frac{\text{W}}{\text{m}^2 \cdot \text{K}} \times (0.2)^2 \times 10^{-4} \text{ m}^2}} \Rightarrow \boxed{\epsilon_{fin} = 44.7}$$

**Start your answer to part (d) here. [4 pts]**

$$\text{Efficiency: } \eta_{fin} = \frac{q_{fin}}{q_{max}} = \frac{q_{fin}}{hA_{fin} \theta_b}$$

$L \rightarrow \infty$  (Infinitely long fin)

$$\Rightarrow \boxed{\eta_{fin} \rightarrow 0}$$

### Problem 3 [30 points]

**Part I (20 Pts):** A metal alloy sphere of 2cm diameter and 20°C of uniform temperature is placed inside a convection oven at  $h = 20 \text{ W}/(\text{m}^2\text{K})$  and  $T_\infty = 800^\circ\text{C}$  for thermal treatment. Neglect radiation heat exchange. *For metal alloy:* thermal conductivity = 200 W/(m·K); density = 2,000kg/m<sup>3</sup>; specific heat = 500 J/(kg·K).

- (a) Can we assume that the sphere is a lumped thermal system? Briefly justify.  
(b) How long does it take (in seconds) for the surface temperature of the sphere to reach 500°C?

**Part II (10 Pts):** After reaching 500°C, the sphere is quenched by dipping into 100 ml of mineral oil at 20°C initial temperature. This process can be treated as convection between the sphere and the oil with  $h = 1,000 \text{ W}/(\text{m}^2\text{K})$  and  $T_\infty$  equal to the average oil temperature. Notice that  $T_\infty$  for oil is rising during this process. Neglect the heat loss to ambient and radiation. *For mineral oil:* density = 1,000 kg/m<sup>3</sup> and specific heat = 1,000 J/(kg·K). Note: 1 ml = 10<sup>-3</sup> m<sup>3</sup>

- (c) Use energy conservation to find the steady state temperature (°C) of the sphere and the oil bath system.  
(d) Derive a differential equation for the sphere temperature (°C) and solve to obtain an expression for sphere temperature as function of time (seconds).

#### **Part I: Start you answer to part (a) here. [7 pts]**

Assumptions: Transient, constant properties, constant h and  $T_\infty$

$$Bi_{lumped} = hL_c / k = h(r_0 / 3) / k = 20 \times (0.01 / 3) / 200 = 3.3 \times 10^{-4} \ll 0.1$$

This system is *lumped*.

#### **Part I: Start your answer to part (b) here. [7 pts]**

From equation sheet or analysis or lumped response:

$$\frac{T(t) - T_\infty}{T_i - T_\infty} = e^{-t/\tau} \quad \text{where } \tau = (\rho_s c_s V_s) / (hA_s) = 167 \text{ [s]}$$

Plug in numbers:

$$(500 - 800) / (20 - 800) = e^{-t/166.7} \Rightarrow \boxed{t = 159 \text{ [s]}}$$

### Problem 3 – continued

#### **Part II: Start your answer to part (c) here. [7 pts]**

From Energy conservation for the sphere/oil system:

Initial energy of sphere + initial energy of oil = Steady-state energy of both

$$\text{Constant at all time} = \rho_s c_s V_s T_s + \rho_{oil} c_{oil} V_{oil} T_{oil} = \rho_s c_s V_s T_{final} + \rho_{oil} c_{oil} V_{oil} T_{final}$$

$$\Rightarrow T_{final} = \frac{(\rho_s c_s V_s T_s + \rho_{oil} c_{oil} V_{oil} T_{oil})|_{t=0}}{\rho_s c_s V_s + \rho_{oil} c_{oil} V_{oil}}$$

$$\Rightarrow \boxed{T_{final} = 39.3^\circ C}$$

#### **Start your answer to part (d) here. [8 pts]**

From previous part:

$$\Rightarrow T_{oil} = \frac{(\rho_s c_s V_s + \rho_{oil} c_{oil} V_{oil}) T_{final} - \rho_s c_s V_s T_s}{\rho_{oil} c_{oil} V_{oil}} \Rightarrow T_{oil} = 40.95 - 0.0419 T_s$$

From energy balance:

$$\rho_s c_s V_s \frac{dT_s}{dt} = -h A_s (T_s - T_{oil}) \Rightarrow \frac{dT_s}{dt} = -0.3(T_s - T_{oil})$$

$$\Rightarrow \boxed{\frac{dT_s}{dt} = -0.313 T_s - 39.3}$$

Solution to this ODE

$$\frac{dT_s}{dt} = -0.313(T_s - 39.3)$$

$$\Rightarrow \frac{d(T_s - 39.3)}{dt} = -0.313(T_s - 39.3)$$

$$\Rightarrow T_s = C_1 e^{-0.313t} + 39.3$$

Use initial condition to determine  $C_1$ :

$$\text{Initial condition: } T_s(t=0) = 500 [^\circ C]$$

$$\Rightarrow \boxed{T_s = 460.7 \times e^{-0.313 \times t} + 39.3} \quad \text{or} \quad \boxed{T_s = 460.7 \times e^{-\frac{t}{3.19}} + 39.3}$$